# A comparative study on head loss characteristics of same pipe material with different diameters in buried pipe distribution system 

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## ABSTRACT

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A research work was conducted on buried pipe distribution systems in two different DTW irrigation schemes located in the villages of Dhitpur and Chongachain the sadar upazilla of Sirajganj district. The main objectives of the study were to determine and compare the head loss characteristics of flow through buried pipes made of cement concrete pipe and having different diameters. Air vents of the buried pipe were used as piezometers for the calculation of hydraulic grade line along the pipe length. The flow rate was measured by a cutthroat flume, placed in the open channel several meters away from the outlet of the buried pipe. This work shows that hydraulic properties of buried pipe such as frictional, entrance and exit losses, as well as friction factor are nonlinearly related to velocity of flow. Frictional, entrance and exit losses, as well as friction factor are significantly smaller in a large diameter pipe compared a small diameter pipe of same material for the same velocity of flow. This study reveals that, for a given velocity, the energy losses are significantly smaller in a large diameter pipe compared a small diameter pipe of same material. Exit loss is greater than the entrance loss except very low flow rates. This study suggests that, as the loss of head in a large diameter pipe compared a small diameter pipe of CC pipes, the former is particularly suitable for long buried pipe lines.

## Introduction

Irrigation for agriculture plays a vital role in increasing crop production in Bangladesh. The performance of an irrigation system depends on engineering, agronomic, organizational and management practices. In fact, irrigation technologies have always been considered as one of the major primary contributors to agricultural development in this country. Obviously, various types of studies are carried out for addressing the issues and problems associated with both the operation and management of irrigation systems. Amongst these, Improvement of performance of water distribution system is the prominent one. For the development of command area of any irrigation project, proper water distribution system and its efficient management play a very important and vital role.

Water distribution in the minor irrigation sector is commonly used of open channel that's made of earthen in Bangladesh and have very low conveyance and distribution efficiencies, resulting in less irrigated area and high maintenance cost. It is
fact that, traditional earthen channel distribution systems confront some physical obstructions and canals suffer from high seepage, leakage and evaporation losses. The buried pipe distribution system (BPDS) may be the best solution to these problems.

In a buried pipe distribution system, the pipelines are placed underground and cultivation can be done above the pipelines without interference to farming operations. If the pipelines are properly installed, they are very durable and the maintenance cost is low. Their placement below ground surface prevents any damage and eliminates water loss by evaporation. The systems are operated under pressure. Therefore, they can be laid uphill and downhill, thus permitting the delivery of water to areas not accessible when open channels are used. They do not become clogged by vegetation and windblown materials. With an underground pipeline system, the DTW need not be located at the highest point of the farm but may be at a location that provides the best water supply. No land needs to be reserved for right-of-way in the buried pipe distribution system (BPDS). This is not only an

[^0]economic advantage but also a practical benefit when a large number of field plots belonging to different individuals are not required to be crossed to distribute water from a pumping well.

Despite the clear advantages and benefits of the buried pipe, some problems have been observed in the systems, for instance, unsatisfactory jointing methods and techniques, frequent leaks, faulty outlet valves, poor hydraulic design (using trial and error method) spillage from air vents, higher initial cost and so on.

Since BPDS uses low-pressure pipes, maximum pressure in the buried pipes should not exceed a limiting value. Therefore, the rate of head loss is an important parameter to be considered in the design of a BPDS. For a given pipe, the head loss per unit length of pipe again depends on discharge through the pipe.

The main objective of this work was to determine major and minor losses in buried pipe distribution systems having different pipe diameters and same pipe materials. The specific objectives were i) to study the friction loss parameters of selected schemes for different flow rates, ii) to determine the head losses at the entrance and exit of a buried pipe system for different discharges, and iii) to compare the head loss characteristics of buried pipe distribution system (BPDS) of different pipe diameters and same pipe materials.

## Materials and Methods

## The study schemes

To study the head loss characteristics of buried pipe with different diameters and same pipe materials of two DTW irrigation schemes were selected. The study sites were located in the villages of Dhitpur and Chongachain the sadar upazilla of Sirajganj district. The sites were about 10 km west of the upazilla headquarter. The diameters of the buried pipes in the study schemes were 20 cm and 25 cmand made of CC respectively.

A schematic diagram showing the hydraulics of flow in a buried pipe system is presented in Figure 1.In this work, the buried pipe distribution systems were run to measure the head losses in the pipe, as well as at the inlet and outlet, for different discharges. The flow rate was measured by a cutthroat flume placed in the open channel several meters away from the outlet of the buried pipe.

## Head loss in pipe

Loss of head in feet of fluid, meaning loss of energy expressed in foot-pounds per pound of fluid, occurs in any flow of fluid through a pipe. The loss is caused by: (1) "pipe friction" along the straight sections of pipe of uniform diameter and uniform roughness and (2) changes in velocity or direction of flow. Losses of these two types are ordinarily referred to respectively as major losses and minor losses.

## Loss of head due to pipe friction

Frictional losses in a pipe are considered to be a major loss. From Darcy-Weisbach formula, loss of head $h_{f}$ is given by
$h_{f}=f \frac{L}{D} \frac{V 2}{2 g}$
Where,
$\mathrm{f}=$ coefficient of friction for pipe, dimensionless
$L=$ length of pipe, $m$
$\mathrm{g}=$ acceleration due to gravity, $\mathrm{m} / \mathrm{s}^{2}$
$\mathrm{V}=$ velocity, $\mathrm{m} / \mathrm{s}$
$\mathrm{D}=$ diameter of pipe, m
$\mathrm{h}_{\mathrm{f}}=$ head loss, m
This formula is of convenient form since it expresses the loss of head in terms of the velocity head in the pipe. Moreover, it is dimensionally correct since $f$ is a numerical factor $\mathrm{L} / \mathrm{D}$ is a ratio of lengths, and $\mathrm{h}_{\mathrm{f}}$ and $\mathrm{V}^{2} / 2 \mathrm{~g}$ are both expressed in units of length.

Value of $f$ depends on pipe materials and velocity of flow. Value of $f$ for different pipe materials and velocities are available in relevant textbooks.

## Methodology

Before starting the experimental work, the buried pipelines, air vents, outlets, storage tank and open channels were properly checked to ensure that they are well in order. The best pipe line of the distribution systems of each study scheme was selected. Flow rate through the buried pipe under study was controlled by adjusting the cap plates of the inlets in the storage tank and the alfalfa valves. After starting the pump, sufficient time was allowed to elapse to stabilize the flow through the buried pipe. A cutthroat flume was placed in the open channel several meters away from the outlet for the measurement of discharge. The flume was installed
with its floor horizontal, length wise and breadth wise.

Air vents of the buried pipe were used for the measurement of pressure head in the pipeline. When the flow through the pipe became steady, piezometric heads, $h_{1}$ and $h_{2}$ were measured with reference to an arbitrary datum as shown in Figure 1. Total head in the storage tank, $\mathrm{H}_{\mathrm{i}}$ causing flow through the pipe and the total head $\mathrm{H}_{0}$ at the outlet were also measured.

Loss of head in the pipe between the two air vents was calculated by subtracting $h_{2}$ from $h_{1}$. From this, loss of head in meter per 100 m length of pipe was calculated. The hydraulic grade line passing through $h_{1}$ and $h_{2}$ was extended backward and forward. From this line, potential head $h_{i}$ in the pipe, just outside the storage tank, was estimated in order to
calculate the entrance loss. Similarly potential head $\mathrm{h}_{0}$ in the pipe just before the outlet was estimated from this hydraulic grade line for the calculation of exit loss.

Entrance loss $\mathrm{h}_{\mathrm{fi}}$ in meter at the inlet was calculated from,
$\mathrm{h}_{\mathrm{fi}}=\mathrm{H}_{\mathrm{i}}-\mathrm{h}_{\mathrm{i}}-\mathrm{V}^{2} / 2 \mathrm{~g}$
Exit loss at the outlet $\mathrm{h}_{\mathrm{fo}}=\mathrm{h}_{\mathrm{o}}-\mathrm{H}_{\mathrm{o}}+\mathrm{V}^{2} / 2 \mathrm{~g}$
where, V is the velocity in meter per second through the buried pipe, $\mathrm{H}_{\mathrm{i}}, \mathrm{h}_{\mathrm{i}}, \mathrm{H}_{\mathrm{o}}$ and $\mathrm{h}_{\mathrm{o}}$ are in meter.

For the estimation of discharge, the upstream flow depth $h_{a}$ and the downstream flow depth $h_{b}$ were measured from the scales attached to the flume. The flow condition was determined from submergence ratio $h_{b} / h_{a}$ and the flow rate was obtained.


Figure 1: A schematic diagram of the hydraulics of flow in a buried pipe

After taking these measurements, for a particular discharge, flow to the selected pipe line was changed by adjusting the alfalfa valves of other pipe lines. Some time was allowed to elapse in order to stabilize the flow in the buried pipe. When the flow in the pipe became steady, $H_{i}, h_{1} h_{2} H_{o}$ were measured for calculation of head losses and $h_{a}$ and $h_{b}$ for discharge. The work was repeated for several variations of discharge.

## Results and Discussion

For each site, hydraulic properties of the buried pipe are calculated from measured data and summarized
in Tables 1. Results obtained in different sites are sequentially presented below in tables and graphs.

## Comparisons of hydraulic properties

The study shows that for the same velocity and same discharge, the frictional losses were different for different pipe diameter. As indicated in FigureA1 and Figure B-1, the frictional loss is greater in 20 cm pipe than that in 25 cm pipe against the same velocity of $0.8 \mathrm{~m} / \mathrm{s}$.

Table A-1: Measurement of discharge data by cutthroat flume and pressure head at different points of 20 cm CC buried pipe.

| Test <br> No. | $\begin{aligned} & \mathrm{h}_{\mathrm{a}} \\ & (\mathrm{~cm}) \end{aligned}$ | $\mathrm{h}_{\mathrm{b}}$ (cm) | $\begin{aligned} & \mathrm{S}=\mathrm{h}_{\mathrm{b}} / \\ & \mathrm{h}_{\mathrm{a}} \end{aligned}$ | Flow condition | $\mathrm{Q}\left(\mathrm{m}^{3} / \mathrm{s}\right)$ | $\mathrm{V}^{2} / 2 \mathrm{~g}$ | $\mathrm{H}_{\mathrm{i}}(\mathrm{m})$ | $\mathrm{h}_{\mathrm{i}}(\mathrm{m})$ | $\mathrm{h}_{1}(\mathrm{~m})$ | $\mathrm{h}_{2}(\mathrm{~m})$ | $\mathrm{h}_{0}(\mathrm{~m})$ | $\mathrm{H}_{0}(\mathrm{~m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 19.20 | 5.70 | 0.30 | Free <br> flow | 0.0435 | 0.098 | 1.938 | 1.577 | 1.423 | 1.070 | 0.8700 | 0.4580 |
| 2 | 18.097 | 5.31 | 0.29 |  | 0.039 | 0.078 | 1.690 | 1.410 | 1.270 | 0.9560 | 0.7760 | 0.4260 |
| 3 | 16.750 | 4.83 | 0.29 |  | 0.032 | 0.053 | 1.35 | 1.135 | 1.035 | 0.808 | 0.676 | 0.394 |
| 4 | 15.24 | 4.39 | 0.28 |  | 0.028 | 0.040 | 1.120 | 0.9495 | 0.8708 | 0.6940 | 0.5933 | 0.366 |
| 5 | 13.97 | 4.05 | 0.29 |  | 0.025 | 0.033 | 0.929 | 0.7910 | 0.7260 | 0.5768 | 0.4910 | 0.3340 |
| 6 | 12.065 | 3.38 | 0.27 |  | 0.0204 | 0.022 | 0.6595 | 0.5555 | 0.5130 | 0.4160 | 0.3600 | 0.2610 |
| 7 | 11.589 | 3.10 | 0.27 |  | 0.017 | 0.015 | 0.5455 | 0.4565 | 0.4240 | 0.3490 | 0.3061 | 0.2350 |
| 8 | 10.319 | 2.80 | 0.27 |  | 0.0139 | 0.0097 | 0.4922 | 0.3955 | 0.3730 | 0.3213 | 0.2916 | 0.2275 |
| 9 | 9.684 | 2.62 | 0.27 |  | 0.0122 | 0.0077 | 0.4542 | 0.3545 | 0.3357 | 0.2926 | 0.2678 | 0.2085 |

Table A-2: Hydraulic properties for different discharges of 20 cm CC buried pipe

| Discharge, <br> $\left(\mathrm{m}^{3} / \mathrm{s}\right)$ | Q | Velocity, $\mathrm{V}(\mathrm{m} / \mathrm{s})$ | Frictional <br> loss, $\mathrm{h}_{\mathrm{f}}(\mathrm{m} / 100 \mathrm{~m})$ | Friction factor, f | Entrance <br> $\mathrm{h}_{\mathrm{fi}}(\mathrm{m})$ |
| :--- | :--- | :--- | :--- | :--- | :--- | loss, | Exit loss, $\mathrm{h}_{\mathrm{fo}}(\mathrm{m})$ |
| :--- |
| 0.0435 |

Table B-1: Measurement of discharge data by cutthroat flume and pressure head at different points of 25 cm CC buried pipe.

| Test No. | $\begin{aligned} & \mathrm{h}_{\mathrm{a}} \\ & (\mathrm{~cm}) \end{aligned}$ | $\begin{aligned} & \mathrm{h}_{\mathrm{b}} \\ & (\mathrm{~cm}) \end{aligned}$ | $\begin{aligned} & \mathrm{S}=\mathrm{h}_{\mathrm{b}} / \\ & \mathrm{h}_{\mathrm{a}} \end{aligned}$ | Flow condition | $\mathrm{Q}\left(\mathrm{m}^{3} / \mathrm{s}\right)$ | $\mathrm{V}^{2} / 2 \mathrm{~g}$ | $\mathrm{H}_{\mathrm{i}}(\mathrm{m})$ | $\mathrm{h}_{\mathrm{i}}(\mathrm{m})$ | $\mathrm{h}_{1}(\mathrm{~m})$ | $\mathrm{h}_{2}(\mathrm{~m})$ | $\mathrm{h}_{0}(\mathrm{~m})$ | $\mathrm{H}_{0}(\mathrm{~m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 20.80 | 6.17 | 0.30 | Free flow | 0.0496 | 0.050 | 1.337 | 1.130 | 1.040 | 0.843 | 0.761 | 0.425 |
| 2 | 19.53 | 5.79 | 0.30 |  | 0.0445 | 0.042 | 1.205 | 1.030 | 0.956 | 0.783 | 0.710 | 0.405 |
| 3 | 18.89 | 5.54 | 0.29 |  | 0.042 | 0.038 | 1.130 | 0.970 | 0.896 | 0.734 | 0.667 | 0.396 |
| 4 | 17.30 | 5.11 | 0.29 |  | 0.037 | 0.029 | 0.925 | 0.786 | 0.728 | 0.602 | 0.548 | 0.346 |
| 5 | 17.10 | 5.05 | 0.29 |  | 0.035 | 0.026 | 0.865 | 0.747 | 0.693 | 0.574 | 0.524 | 0.337 |
| 6 | 15.87 | 4.57 | 0.29 |  | 0.03 | 0.020 | 0.763 | 0.678 | 0.634 | 0.537 | 0.497 | 0.325 |
| 7 | 15.28 | 4.4 | 0.29 |  | 0.027 | 0.05 | 0.640 | 0.575 | 0.537 | 0.453 | 0.418 | 0.272 |
| 8 | 13.34 | 3.87 | 0.29 |  | 0.023 | 0.011 | 0.516 | 0.505 | 0.473 | 0.403 | 0.373 | 0.255 |
| 9 | 12.07 | 3.32 | 0.27 |  | 0.09 | 0.008 | 0.474 | 0.393 | 0.365 | 0.304 | 0.278 | 0.215 |

Table B-2: Hydraulic properties for different discharges of 25 cm CC buried pipe




Figure A.2: Relationship between discharge and frictional loss for 20 cm CC


Figure A.3: Relationship between velocity and friction factor for 20 cm CC buried pipe


Figure B.2: Relationship between discharge and frictional loss for 25 cm CC buried pipe


Figure B.3: Relationship between velocity and friction factor for 25 cm CC buried pipe


Figure A.4: Relationship between velocity and Entrance loss for 20 cm CC buried pipe


Figure A.5: Relationship between velocity and Exit loss for 20 cm CC buried pipe

Similarly, for the same discharge of $0.03 \mathrm{~m}^{3} / \mathrm{s}$ (Figure A. 2 and Figure B.2) frictional loss is again greater in the 20 cm CC pipe than that in 25 cm CC pipe.

For the same velocity of flow, friction factor varies for different pipe diameters (Figure A. 3 and Figure B.3). The friction factor is greater in 25 cm pipe than that in 20 cm pipe against the same velocity of 0.8 $\mathrm{m} / \mathrm{s}$.

For the same velocity of flow, entrance and exit losses vary for different pipe diameters (Figure A.4, Figure B.4, Figure A. 5 and Figure B.5). Entrance loss is greater in 20 cm pipe than that in 25 cm pipe against the same velocity of $0.8 \mathrm{~m} / \mathrm{s}$. The exit loss


Figure B.4: Relationship between velocity and Entrance loss for 25 cm CC buried pipe


Figure B.5: Relationship between velocity and Exit loss for 25 cm CC buried pipe
for a velocity of $0.8 \mathrm{~m} / \mathrm{s}$ is greater in 25 cm pipe than that in 20 cm pipe.

From these results and discussion, it can be said that, the frictional loss nonlinearly related to both velocity and discharge. For the buried pipes of same material, frictional loss decreases with the increase of pipe diameter for the same velocity of flow.

The friction factor decreases nonlinearly with the increase of velocity of flow in a given buried pipe. For the pipes of same material, friction factor increases with the increase of pipe diameter.

The entrance loss initially decreases up to a certain increase of velocity and then it increases with the increase of velocity. For the pipes of same material,
entrance loss increases with the decrease of pipe diameter for the same velocity.

Exit loss varies nonlinearly with the velocity of flow. For the buried pipes of same material, it increases; it increases with the decrease of the pipe diameter.

## Conclusions

Hydraulic properties of buried pipe, such as frictional, entrance and exit losses as well as friction factor are nonlinearly related to velocity of flow. Frictional, entrance and exit losses are significantly smaller in a large diameter pipe compared to a small diameter pipe of same mater for a given velocity of flow. Exit loss is greater than the entrance loss except very low flow rates. As the loss of head is significantly smaller in a large diameter compared to a small diameter in CC pipe, the former is particularly suitable for long buried pipe lines.

## Recommendations

Similar study should be carried out in other buried pipe irrigation schemes where pipes of other diameters are used. Large diameter in CC pipe is found to be superior in terms of pipe material of hydraulic properties. However, economic analyses need to be carried out to determine which of these is profitable to use in buried pipe distribution system.

## References

Ahmed, C. H. (1984). Bogura Underground Asbestos Cement Pipe System. An Economic analysis. Proceedings of Workshop on Improved Distribution System for Minor Irrigation in Bangladesh held at the Bangladesh Agricultural Research Council (BARC) on 8-9 July 1984.
BARI, (1988). Bangladesh Agricultural Research Institute (BARI). Annual Report (1987-88), Joydebpur, Gazipur, Bangladesh.
Bentum, R. (1992). Low Pressure Buried Pipe Distribution Systems for Surface Irrigation. M. Phil Thesis. Loughborough University of Technology, UK.
Bentum, R. \& Smout, I. K. (1993).Planning and Design of Buried Pipe Distribution System for Surface Irrigation- The $15^{\text {th }}$ congress on ICID Conference, The Hoque, The Netherlands.
Bentum, R. Smout, I. K., Rashid, M. H. \& Mridha, M. A. K. (1990). Interim Report on Desk Study Research into Buried Pipe Distribution Systems for Irrigation. Overseas Development Administration (UK) Project R4575: Water, Engineering and Development Centre Loughborough, UK.

Brod, S. I. (1990). Tour Report from 16 December 1989 to 14 June 1990. IDA-DTW II Project. Sir MacDonald International Ltd. Bangladesh Agricultural Development Cooperation, Bangladesh.
Gisselquist, D. (1986). Low Cost Concerete Pipe Irrigation System for DTWS, STWs and LLPs. Draft paper, Bangladesh.
Gisselquist, D. (1989). Demonstrating Command Area Development.Tangail Agricultural Development Project, BRDB/GTZ.
Hannan, A. \&Haque, R. (1984).Observations from Tour of Indian Buried Pipe Systems. Proceedings of a Workshop on Improved Distribution Systems for Minor Irrigation in Bangladesh held at Bangladesh Agricultural Research Council (BARC) on 8-9 July 1984. Farm Gate, Dhaka, Bangladesh.
James, L. G. (1988). Principles of Farm Irrigation System Design.Wiley.
Jenkins, D. (1983). Irrigation water distribution system for tubewells and low lift pumps in Bangladesh, Dhaka, Bangladesh: United States Agency for International Development.
Macdonald, (1992). Mott MacDonald International Ltd. Main Report: 1983-1992. IDA Deep TubewellI I Project, Bangladesh.
Matin, M. A. (1990). Research Projects Under Irrigation Management Training Programme. Rural Development Academy (RDA), Bogra, Bangladesh.
Meerriam, J. L. (1985). Demand Irrigation Schedule Concrete Pipeline Pilot Project. Final Report. Mahaweli Development Board.p. 10
Michael, A. M. (1978). Irrigation Theory and Practices Vikas, New Delhi.
Michael, A. M. (1986). Irrigation Theory and Practice.Indian Agricultural Research Institute, New Delhi, India.
Michael, A. M. (1987). Assessment of Research and Pilot Demonstration on Water Distribution Systems and Crop Water Requirement in Bangladesh. BARC, Windrock International Institute for Agricultural Development, Bangladesh.
Moigne, G. L., Shawki Barghouti \& Herve Plusquellec (1989).Technological and Institutional Innovation in Irrigation, World Bank.
Palmer-Jones, R. W. \& Mandal, M. A. S. (1988). Clubs, Capitalists or Cooperatives: A conceptual frame work for Deep Tubewell Management in Tangail District. Consultancy report prepared for Tangail Agricultural Development Project: Bangladesh Rural Development Board/German Agency for Technical Cooperation, Dhaka.
Pluje, J. (1981). Short Report of Experimental Underground Low Pressure Pipe System for Irrigation Water Distribution. Bogra, Bangladesh.
Rahman, M. (1990). Internal Draft Report on Spun Pipe Production Tangail Agricultural Development Project (TADP). TADP/GTZ, Bailla, Mymensingh Road, Tangail, Bangladesh.

Rahman, M. A. (1987). Success stories, Tangail Agricultural Development Project. Bangladesh Rural Development Board (BRDB). Palli Bhaban, 5 Kawran Bazar, Dhaka, Bangladesh.
Rahman, M. A. (1989). Success Stories: Tangail Agricultural Development Project. Bangladesh Rural Development Board (BRDB). PalliBhaban, 5 Kawran Bazar, Dhaka, Bangladesh.
Georgi, (1989). Research Project under Tangail Agricultural Development Project, Tangail, Bangladesh.
Rashid, M. H. \& Mridha, M. A. K. (1990). Interim Field work Report: 1989-90 Irrigation Season. Research into Buried Pipe Distribution Systems for Irrigation.Overseas Development Administration (ODA), UK and Bangladesh Agricultural Research Institute (BARI).

Rashid, M. H. \& Mridha, M. A. K. (1992). Final Report: 1989-91. Research into Buried Pipe Distribution Systems for Irrigation. Overseas Development Administration (ODA), UK and Bangladesh Agricultural Research Institute.
UNDP (1982).Ground Water Survey.The Hydrogeological conditions of Bangladesh, Groundwater Circle. Bangladesh Water Development Board (BWDB), Dhaka, Bangladesh.
Worstell, R. V. (1979). An Experimental Buried Multiset Irrigation System-Transactions of the RSAE, 1979.p. 10,

Yadav, R. C. (1985). Conjunctive use of Lined Canals and Underground pipelines for water conveyance under gravity irrigation. Journal of Agricultural Engineering Research.


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